

Multibinit lattice part: From ab-initio data to predictive lattice potentials

ABINIT Developer Workshop 2021

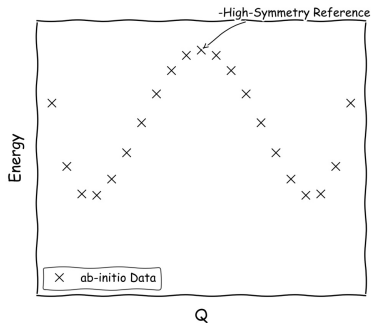
M. Schmitt, L. Bastogne, J. Bieder and Ph. Ghosez

Theoretical Materials Physics, CESAM, Université de Liège, B-4000 Liège, Belgium

- Ab-Initio still limited to somewhat short time and length scales.
- State of the art for large scale MD: Reactive Force Fields, and empirical potentials.
- Current research effort: Effective potentials fitted on ab-initio data: Close the gap between ab-initio and effective potentials !
- Our approach: Reproduce the ab-initio potential energy surface (PES) by a polynomial fit → second-principles.

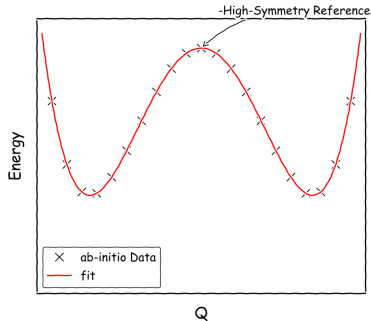
Second-Principles Effective Potential from Ab-Initio Data

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$$E = E_0 + c_2 Q^2 + c_3 Q^3 + c_4 Q^4 \dots$$

- 1** **Model definition**

- 2** **Training set generation**

- 3** **Model Generation & Fit**

- 4** **Testing/validation**

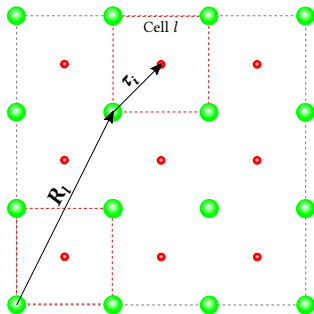
- 5** **Predictions & analysis tools**

Lattice Description

Reference Structure: $\{r_0\}$

 Reference Unit-Cell

 Simulation Box

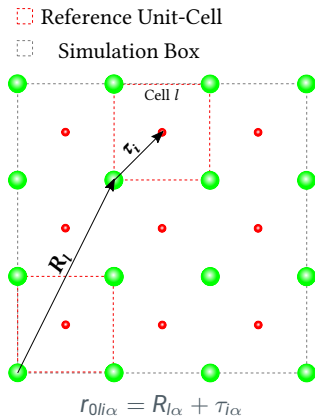


$$r_{0l\alpha} = R_{l\alpha} + \tau_{l\alpha}$$

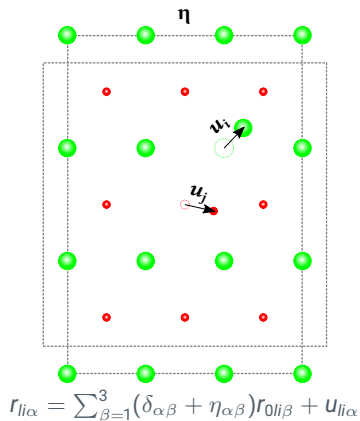
Escorihuela-Sayaler et al., Phys. Rev. B **95**, 094115
J. Wojdel et al., J. Phys. Condens. Matter **25** (2013) 305401

Lattice Description

Reference Structure: $\{\mathbf{r}_0\}$



Distorted structure: $\{\mathbf{r}\}$



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Modifications of the energy around the reference structure

$$E_{\text{tot}}(\{\mathbf{u}_i\}, \boldsymbol{\eta}) = E_0(\{\mathbf{r}_0\}, 0) + E_p(\{\mathbf{u}_i\}) + E_s(\boldsymbol{\eta}) + E_{sp}(\{\mathbf{u}_i\}, \boldsymbol{\eta})$$

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Atomic displacements

$$E_p(\{\mathbf{u}_i\}) = E_p^{\text{Harm}}(\{\mathbf{u}_i\}) + E_p^{\text{Anharm}}(\{\mathbf{u}_i\})$$

$$K_{\alpha\beta\gamma\dots}^{(n)} = \left. \frac{\partial^n E_{\text{tot}}}{\partial u_{i\alpha} \partial u_{j\beta} \dots} \right|_{\boldsymbol{\eta}=0}$$

$K^{(2)}$: Inter-atomic force constant

Modifications of the energy around the reference structure

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Strain deformation

$$E_s(\boldsymbol{\eta}) = E_s^{\text{Harm}}(\boldsymbol{\eta}) + E_s^{\text{Anharm}}(\boldsymbol{\eta})$$

$$C_{ab\dots}^{(m)} = \left. \frac{1}{N} \frac{\partial^m E_{\text{tot}}}{\partial \eta_a \partial \eta_b \dots} \right|_{\mathbf{u}_i=0}$$

$C^{(2)}$: Elastic constant

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Strain-phonon coupling

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$$\Lambda_{i\alpha a\dots}^{(m,n)} = \frac{\partial^m E_{\text{tot}}}{\partial u_{i\alpha} \partial \eta_a \dots}$$

$\Lambda^{(1,1)}$: force-response internal strain tensor

Second-principles

Modifications of the energy around the reference structure

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$K^{(2)}$: Inter-atomic force constant

- All atomic degrees of freedom are included
- $K^2, C^2, \Lambda^{(1,1)}$ can be calculated **directly** from DFPT
- **Anharmonic** term parameters: fitted to reproduce representative ab-initio data (TS)

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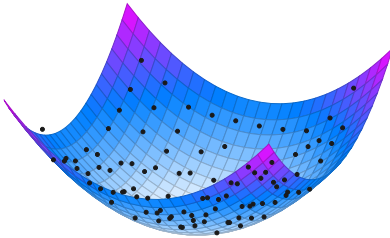
$\Lambda^{(1,1)}$: force-response internal strain tensor

λ	1 st order	2 nd order		
		$\mathbf{u}$	$\boldsymbol{\eta}$	$\boldsymbol{\varepsilon}$
$\mathbf{u}$	f	K	Λ	Z^*
$\boldsymbol{\eta}$	σ	Λ	C	e^0
$\boldsymbol{\varepsilon}$	P	Z^*	e^0	ε^∞

Read from a .DDB file

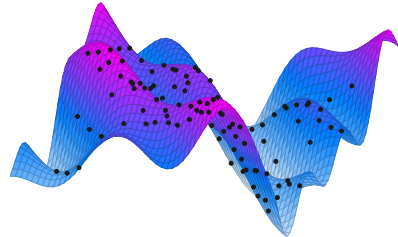
Choice of TS generation strategy

Two scenarios



One minimum to explore

- Easy to explore with random structures

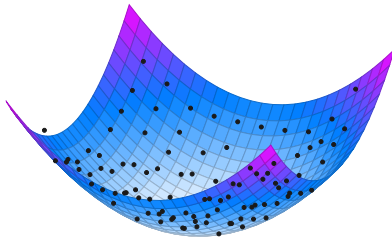


Several local minima to explore:

- Hard to explore all the minima with random structures

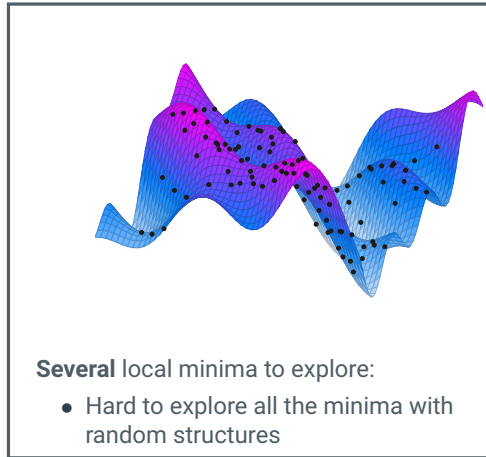
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2 Training set generation

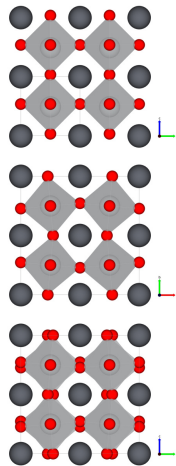
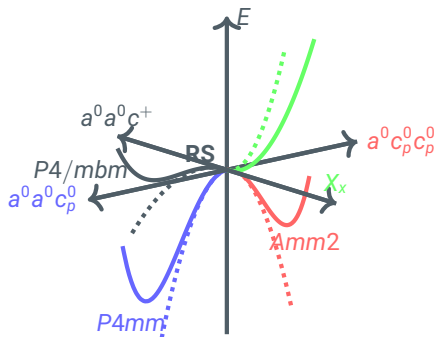
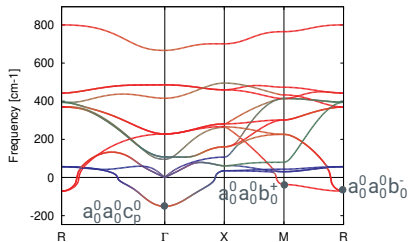
- Training set generation
- Exploration of energy landscape: Interpolations & extrapolations
- Exploration of energy landscape: Phonon & strain noise on minima
- Exploration of energy landscape: Phonon & strain noise on path

3 Model Generation & Fit

4 Testing/validation

5 Predictions & analysis tools

Training set generation I Identification of instabilities

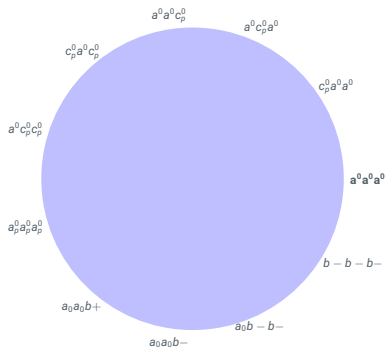
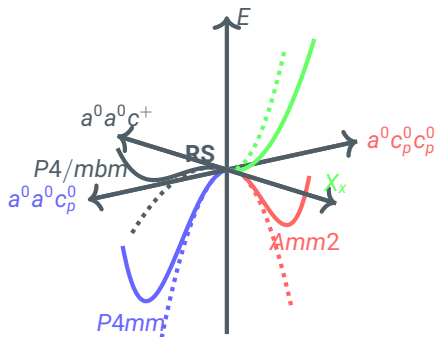
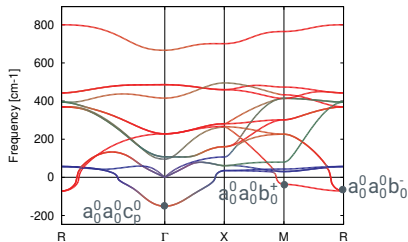


$$\Gamma: a_0^0 a_0^0 c_p^0$$

$$M: a_0^0 a_0^0 b_0^+$$

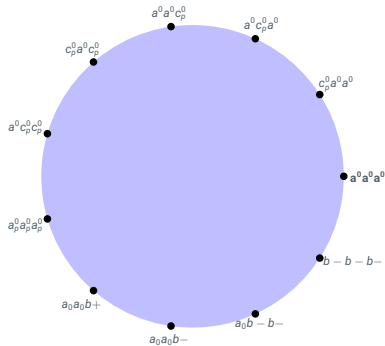
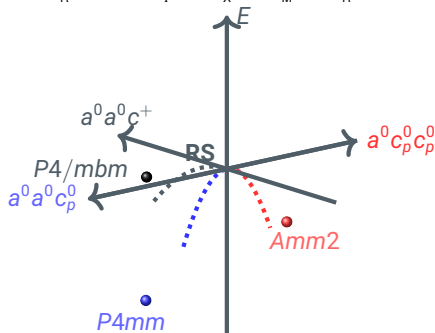
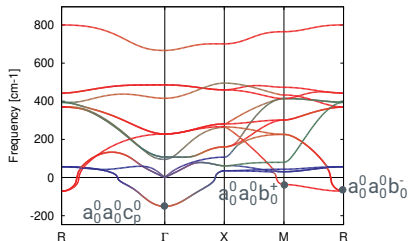
$$R: a_0^0 a_0^0 b_0^-$$

Identification of **instabilities** (negative curvature): anharmonicities are required to build a second-principles potential



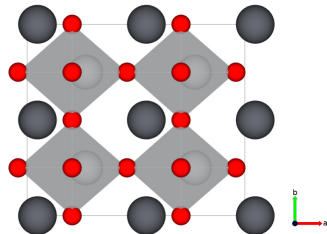
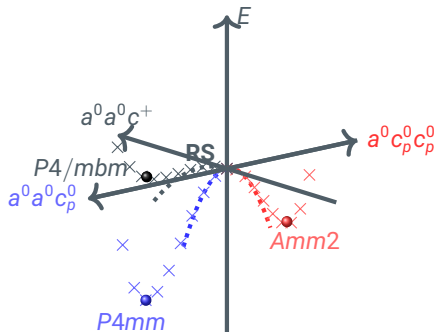
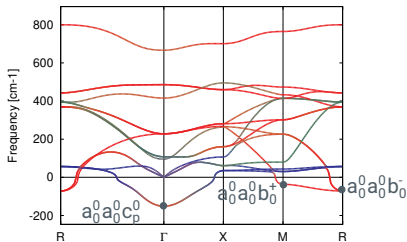
Identification of **instabilities** (negative curvature): reduce the complete B-O surface to the subspace of interest

Training set generation I Identification of instabilities



Identification of **instabilities** (negative curvature): Relaxation towards local minima

TS generation Interpolations & extrapolations

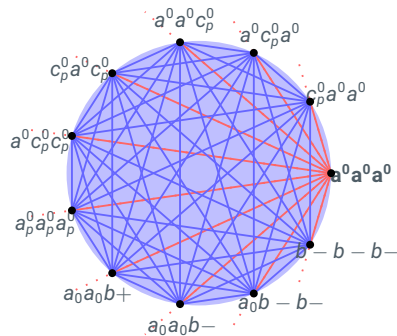
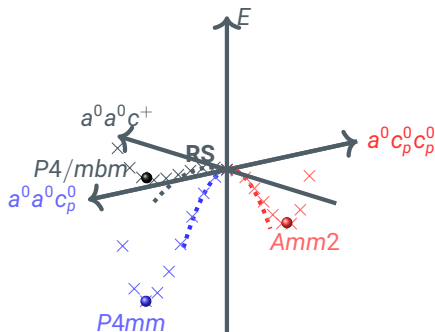
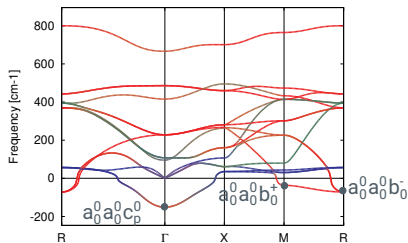


- **Linear Interpolation:** connecting all minima ($\alpha_{\max} = 1$):

$$\alpha S_1 + \frac{(\alpha_{\max} - \alpha) S_2}{\alpha_{\max}}, \alpha \in [0; \alpha_{\max}[\quad (1)$$

- **Extrapolation** after minima ($\alpha_{\max} > 1$)

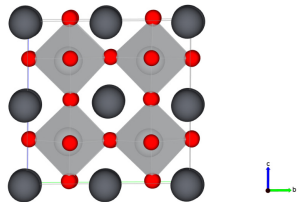
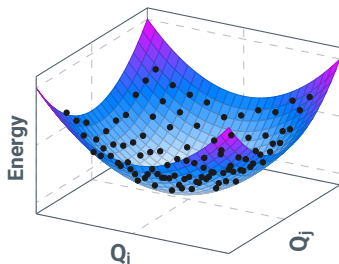
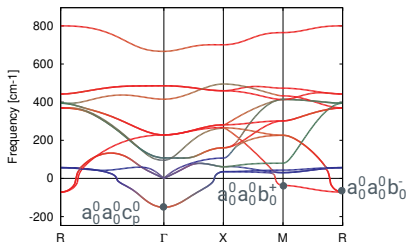
TS generation Interpolations & extrapolations



Command in AGATE

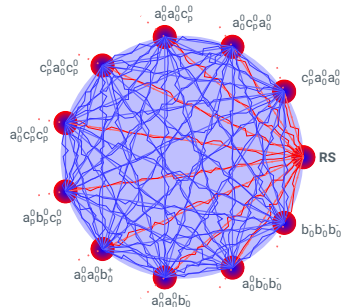
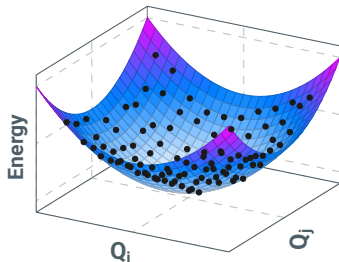
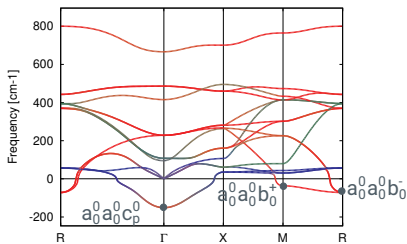
```
:interpolate npoints=· amplitude=·
```

TS generation Phonon & strain noise



- Thermal population of **stable phonons modes** on minima and paths
- **Strain noise** on minima and paths

TS generation Phonon & strain noise

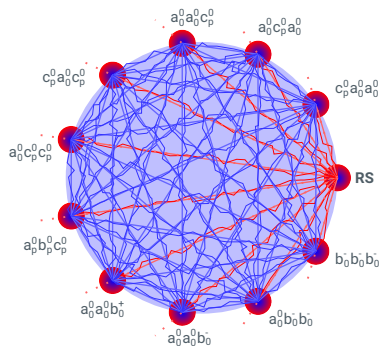


Command in AGATE

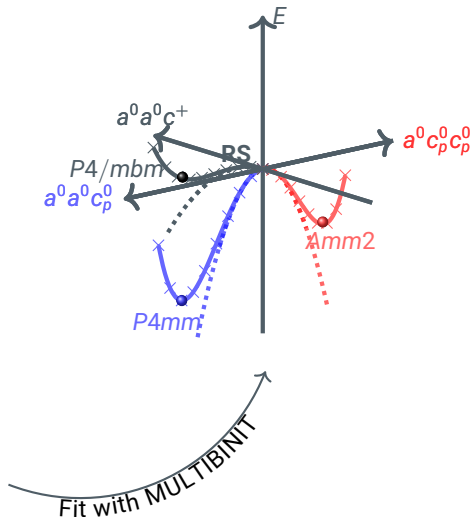
:thermalpop trajectory=

- randomType=Uniform/Normal
- statistics=Classical/Quantum
- iso=: tetra=: shear=:
- temperature=

From training set to atomistic model



- Interpolations: RS to minima
- Interpolations: between minima
- ... Extrapolations
-  Phonon and strain noise around minima
-  Phonon and strain noise on RS - minima paths
-  Phonon and strain noise on minima - minima paths



- 1 Model definition
- 2 Training set generation
- 3 **Model Generation & Fit**
 - Expansion Generation
 - An UNDERDETERMINED system ...
 - Fit and Select important coefficients
 - Outlook: Learn from machine learning
- 4 Testing/validation
- 5 Predictions & analysis tools

Anharmonic Polynomial Expansion

$$E_{\text{tot}}(\{\mathbf{u}_i\}, \eta) = E_0(\{\mathbf{r}_0\}, 0) + E_p(\{\mathbf{u}_i\}) + E_s(\eta) + E_{sp}(\{\mathbf{u}_i\}, \eta)$$

Atomic displacements

$$E_p(\{\mathbf{u}_i\}) = E_p^{\text{Harm}}(\{\mathbf{u}_i\}) + E_p^{\text{Anharm}}(\{\mathbf{u}_i\})$$

Strain deformation

$$E_s(\eta) = E_s^{\text{Harm}}(\eta) + E_s^{\text{Anharm}}(\eta)$$

Strain-phonon coupling

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$$+ K_{ijklmnop}^{(4)}(u_{i\alpha} - u_{j\alpha})(u_{k\beta} - u_{l\beta})(u_{m\gamma} - u_{n\gamma})(u_{o\delta} - u_{p\delta})$$

$$+ \dots$$

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$$E_{sp}^{\text{Anharm}} = \Lambda_{ijkl}^{(2,1)}(u_{i\alpha} - u_{j\alpha})(u_{k\beta} - u_{l\beta})\eta_\gamma \\ + \Lambda_{ij}^{(1,2)}(u_{i\alpha} - u_{j\alpha})\eta_\beta\eta_\gamma \\ + \dots$$

- $$K_{BX}^{(4)}(u_{Bx} - u_{Xx})^4 = K_{BX[100]}^{(4)}(u_{Bx} - u_{X[100]x})^4 \in t_x$$



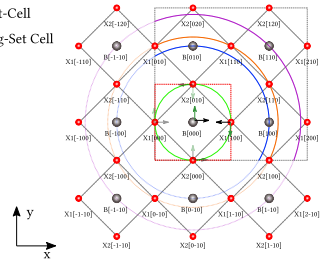
Anharmonic Polynomial Expansion

- Use symmetry to group terms to symmetry adapted terms: t

$$K_{BX}^{(4)}(u_{Bx} - u_{Xx})^4 = K_{BX[100]}^{(4)}(u_{Bx} - u_{X[100]x})^4 \in t$$

- Input:

- Reference Unit-Cell
- 2x2x2 Training-Set Cell
- rcut: $0.5a$
- rcut: a
- rcut: $\sqrt{\frac{5}{4}}a$
- rcut: $\sqrt{2}a$



Anharmonic Polynomial Expansion

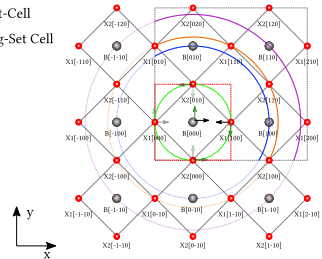
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- Input:

- Order range of the expansion. Typically 3 to 4.

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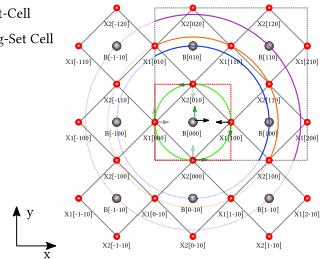
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- Input:

- Order range of the expansion. Typically 3 to 4.
- Interaction Range: Maximum distance for $(u_i - u_j)$ pairs

- Reference Unit-Cell
- 2x2x2 Training-Set Cell

- rcut: $0.5a$
- rcut: a
- rcut: $\sqrt{\frac{5}{4}}a$
- rcut: $\sqrt{2}a$



Anharmonic Polynomial Expansion

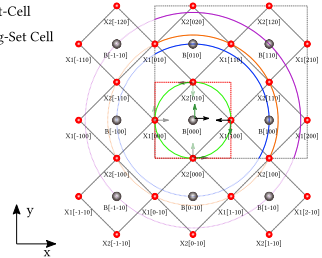
- Use symmetry to group terms to symmetry adapted terms: t

$$K_{BX}^{(4)}(u_{Bx} - u_{Xx})^4 = K_{BX[100]}^{(4)}(u_{Bx} - u_{X[100]x})^4 \in t$$

- Input:

- Order range of the expansion. Typically 3 to 4.
- Interaction Range: Maximum distance for $(u_i - u_j)$ pairs
- Including Anharmonic strain and strain-phonon coupling

- Reference Unit-Cell
- 2x2x2 Training-Set Cell
- rcut: $0.5a$
- rcut: a
- rcut: $\sqrt{\frac{5}{4}}a$
- rcut: $\sqrt{2}a$



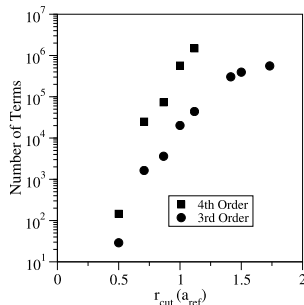
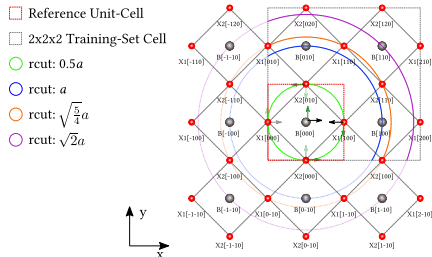
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- Maximum order of strain in strain-phonon coupling



Anharmonic Polynomial Expansion

- Use symmetry to group terms to symmetry adapted terms: t

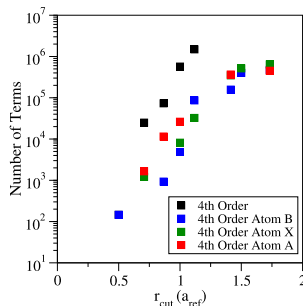
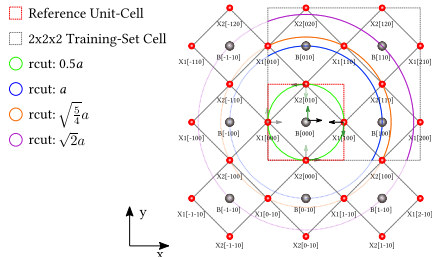
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- Input:

- Order range of the expansion. Typically 3 to 4.
- Interaction Range: Maximum distance for $(u_i - u_j)$ pairs
- Including Anharmonic strain and strain-phonon coupling
- Maximum order of strain in strain-phonon coupling

- Reduce number of terms by only including terms of form

$$K_{ijkl}^{(3)}(u_{i\alpha} - u_{j\alpha})(u_{i\beta} - u_{k\beta})(u_{i\gamma} - u_{l\gamma})$$



System of linear equations $B = AX$

Fitting the anharmonic expansion

System of linear equations $B = AX$

$$\begin{pmatrix}
 E_{DFT}^{(1)} - E_{Har}^{(1)} \\
 E_{DFT}^{(2)} - E_{Har}^{(2)} \\
 \vdots \\
 E_{DFT}^{(N^{TS})} - E_{Har}^{(N^{TS})} \\
 F_{1x}^{DFT(1)} - F_{1x}^{Har(1)} \\
 F_{1y}^{DFT(1)} - F_{1y}^{Har(1)} \\
 \vdots \\
 F_{n_{TSz}at}^{DFT(N^{TS})} - F_{n_{TSz}at}^{Har(N^{TS})} \\
 \vdots \\
 S_1^{DFT(1)} - S_1^{Har(1)} \\
 S_2^{DFT(1)} - S_2^{Har(1)} \\
 \vdots \\
 S_6^{DFT(N^{TS})} - S_6^{Har(N^{TS})}
 \end{pmatrix} = \begin{pmatrix}
 t_1(1) & t_2(1) & t_3(1) & \cdots & t_N(1) \\
 t_1(2) & t_2(2) & t_3(2) & \cdots & t_N(2) \\
 \vdots & \vdots & \vdots & \vdots & \vdots \\
 t_1^{(N^{TS})} & t_2^{(N^{TS})} & t_3^{(N^{TS})} & \cdots & t_N^{(N^{TS})} \\
 \frac{\partial t_1}{\partial u_{1x}}(1) & \frac{\partial t_2}{\partial u_{1x}}(1) & \frac{\partial t_3}{\partial u_{1x}}(1) & \cdots & \frac{\partial t_N}{\partial u_{1x}}(1) \\
 \frac{\partial t_1}{\partial u_{1y}}(1) & \frac{\partial t_2}{\partial u_{1y}}(1) & \frac{\partial t_3}{\partial u_{1y}}(1) & \cdots & \frac{\partial t_N}{\partial u_{1y}}(1) \\
 \vdots & \vdots & \vdots & \vdots & \vdots \\
 \frac{\partial t_1}{\partial u_{n_{TSz}at}}(N^{TS}) & \frac{\partial t_2}{\partial u_{n_{TSz}at}}(N^{TS}) & \frac{\partial t_3}{\partial u_{n_{TSz}at}}(N^{TS}) & \cdots & \frac{\partial t_N}{\partial u_{n_{TSz}at}}(N^{TS}) \\
 \frac{\partial t_1}{\partial \eta_1}(1) & \frac{\partial t_2}{\partial \eta_1}(1) & \frac{\partial t_3}{\partial \eta_1}(1) & \cdots & \frac{\partial t_N}{\partial \eta_1}(1) \\
 \frac{\partial t_1}{\partial \eta_2}(1) & \frac{\partial t_2}{\partial \eta_2}(1) & \frac{\partial t_3}{\partial \eta_2}(1) & \cdots & \frac{\partial t_N}{\partial \eta_2}(1) \\
 \vdots & \vdots & \vdots & \vdots & \vdots \\
 \frac{\partial t_1}{\partial \eta_6}(N^{TS}) & \frac{\partial t_2}{\partial \eta_6}(N^{TS}) & \frac{\partial t_3}{\partial \eta_6}(N^{TS}) & \cdots & \frac{\partial t_N}{\partial \eta_6}(N^{TS})
 \end{pmatrix} \begin{pmatrix} \theta_1 \\ \theta_2 \\ \theta_3 \\ \vdots \\ \theta_N \end{pmatrix}$$

Fitting the anharmonic expansion

System of linear equations $B = AX$

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 E_{DFT}^{(1)} - E_{Har}^{(1)} \\
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 F_{1y}^{DFT(1)} - F_{1y}^{Har(1)} \\
 \vdots \\
 F_{n_{at}z}^{DFT(N^{TS})} - F_{n_{at}z}^{Har(N^{TS})} \\
 \vdots \\
 S_1^{DFT(1)} - S_1^{Har(1)} \\
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 \vdots & \vdots & \vdots & \vdots & \vdots \\
 t_1^{(N^{TS})} & t_2^{(N^{TS})} & t_3^{(N^{TS})} & \dots & t_N^{(N^{TS})} \\
 \frac{\partial t_1}{\partial u_{1x}}(1) & \frac{\partial t_2}{\partial u_{1x}}(1) & \frac{\partial t_3}{\partial u_{1x}}(1) & \dots & \frac{\partial t_N}{\partial u_{1x}}(1) \\
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 \vdots & \vdots & \vdots & \vdots & \vdots \\
 \frac{\partial t_1}{\partial u_{n_{at}z}}(N^{TS}) & \frac{\partial t_2}{\partial u_{n_{at}z}}(N^{TS}) & \frac{\partial t_3}{\partial u_{n_{at}z}}(N^{TS}) & \dots & \frac{\partial t_N}{\partial u_{n_{at}z}}(N^{TS}) \\
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 \frac{\partial t_1}{\partial \eta_2}(1) & \frac{\partial t_2}{\partial \eta_2}(1) & \frac{\partial t_3}{\partial \eta_2}(1) & \dots & \frac{\partial t_N}{\partial \eta_2}(1) \\
 \vdots & \vdots & \vdots & \vdots & \vdots \\
 \frac{\partial t_1}{\partial \eta_6}(N^{TS}) & \frac{\partial t_2}{\partial \eta_6}(N^{TS}) & \frac{\partial t_3}{\partial \eta_6}(N^{TS}) & \dots & \frac{\partial t_N}{\partial \eta_6}(N^{TS})
 \end{pmatrix} \begin{pmatrix} \theta_1 \\ \theta_2 \\ \theta_3 \\ \vdots \\ \theta_N \end{pmatrix}$$

→ Way too many independent coefficients to determine.

→ Select *some important* terms and fit their coefficients.

Step forward selection procedure

$$\min ||B - AX||^2 \text{ and } \min \theta_i \neq 0$$

Step forward selection procedure

$$\min ||B - AX||^2 \text{ and } \min \theta_i \neq 0$$

$$G(\Theta_p, TS) = \frac{1}{N_1} \sum_s \frac{1}{\Omega^1(s)} (E_{DFT}^{Anh}(s) - E^{Anh}(\Theta_p, s))^2 + \frac{1}{N_2} \sum_{si\alpha} (F_{DFTi\alpha}^{Anh}(s) - F_{i\alpha}^{Anh}(\Theta_p, s))^2 \\ + \frac{1}{N_3} \sum_{s\kappa} \Omega^2(s) (S_{DFT,\kappa}^{Anh}(s) - S_{\kappa}^{Anh}(\Theta_p, s))^2$$

Step forward selection procedure

$$\min ||B - AX||^2 \text{ and } \min \theta_i \neq 0$$

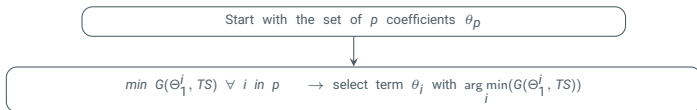
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Start with the set of p coefficients θ_p

Step forward selection procedure

$$\min ||B - AX||^2 \text{ and } \min \theta_i \neq 0$$

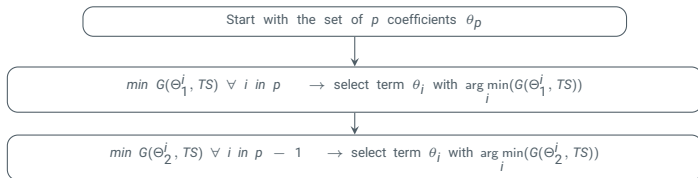
$$G(\Theta_p, TS) = \frac{1}{N_1} \sum_s \frac{1}{\Omega^1(s)} (E_{DFT}^{Anh}(s) - E^{Anh}(\Theta_p, s))^2 + \frac{1}{N_2} \sum_{si\alpha} (F_{DFTi\alpha}^{Anh}(s) - F_{i\alpha}^{Anh}(\Theta_p, s))^2 \\ + \frac{1}{N_3} \sum_{s\kappa} \Omega^2(s) (S_{DFT,\kappa}^{Anh}(s) - S_{\kappa}^{Anh}(\Theta_p, s))^2$$



Step forward selection procedure

$$\min ||B - AX||^2 \text{ and } \min \theta_i \neq 0$$

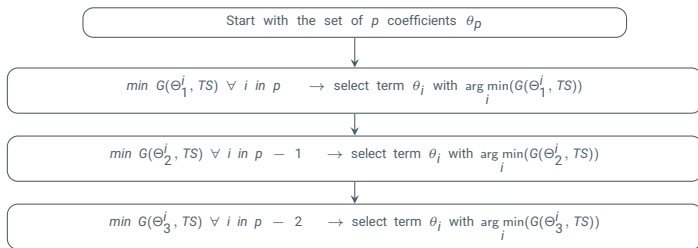
$$G(\Theta_p, TS) = \frac{1}{N_1} \sum_s \frac{1}{\Omega^1(s)} (E_{DFT}^{Anh}(s) - E^{Anh}(\Theta_p, s))^2 + \frac{1}{N_2} \sum_{si\alpha} (F_{DFTi\alpha}^{Anh}(s) - F_{i\alpha}^{Anh}(\Theta_p, s))^2 \\ + \frac{1}{N_3} \sum_{s\kappa} \Omega^2(s) (S_{DFT,\kappa}^{Anh}(s) - S_{\kappa}^{Anh}(\Theta_p, s))^2$$



Step forward selection procedure

$$\min ||B - AX||^2 \text{ and } \min \theta_i \neq 0$$

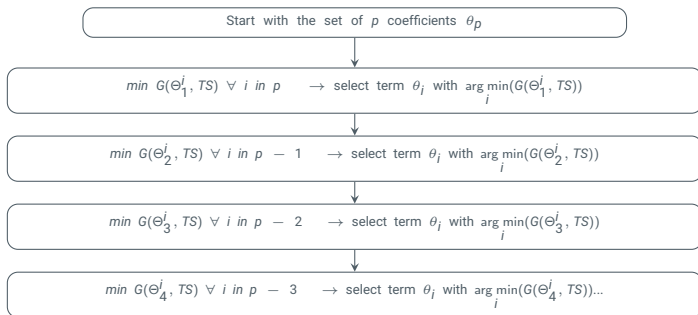
$$G(\Theta_p, TS) = \frac{1}{N_1} \sum_s \frac{1}{\Omega^1(s)} (E_{DFT}^{Anh}(s) - E^{Anh}(\Theta_p, s))^2 + \frac{1}{N_2} \sum_{s_{i\alpha}} (F_{DFTi\alpha}^{Anh}(s) - F_{i\alpha}^{Anh}(\Theta_p, s))^2 \\ + \frac{1}{N_3} \sum_{s_{\kappa}} \Omega^2(s) (S_{DFT, \kappa}^{Anh}(s) - S_{\kappa}^{Anh}(\Theta_p, s))^2$$



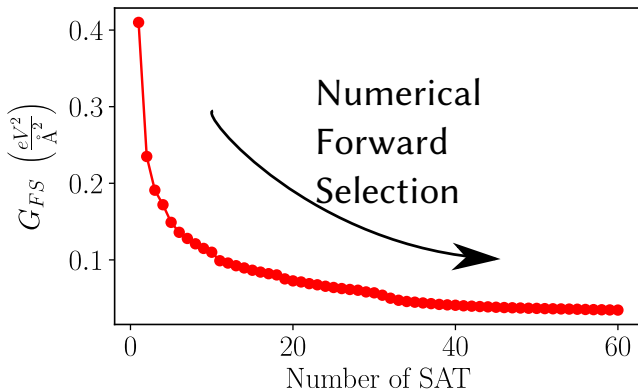
Step forward selection procedure

$$\min ||B - AX||^2 \text{ and } \min \theta_i \neq 0$$

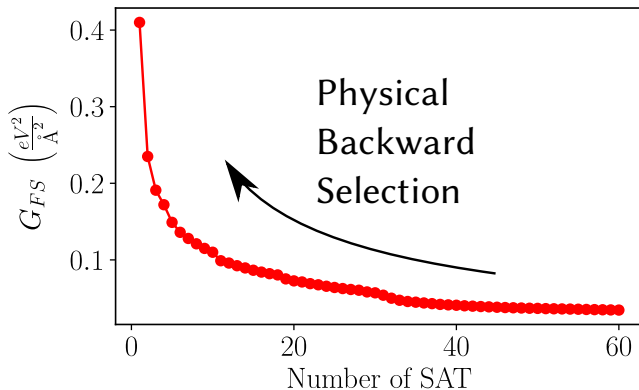
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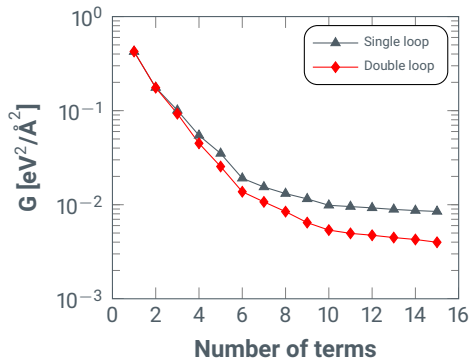
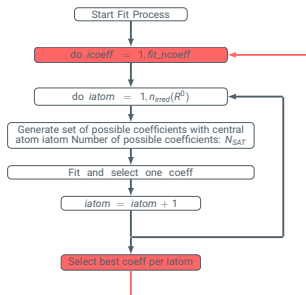
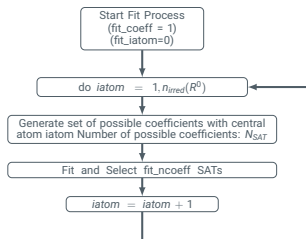
Step forward selection procedure



Step forward selection procedure



Different fitting schemes



Outlook: Learn from machine learning

- Use methods known in **compressive sensing** techniques: LASSO and Elastic/Net Penalizations
- Add penalization term to least squares operator, rewarding solutions with few non zero coefficients.
- Use filtering techniques to eject terms with little corelation to the ab-initio data from fit and selection procedure.



LASSO

$$\hat{X} = \arg \min_x (||B - AX||^2 + \alpha ||X||_1)$$

Elastic Net

$$\hat{X} = \arg \min_x (||B - AX||^2 + \alpha_1 ||X||_1 + \alpha_2 ||X||^2)$$

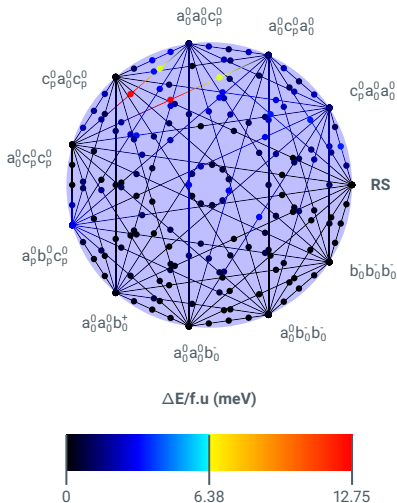
Pearson Correlation

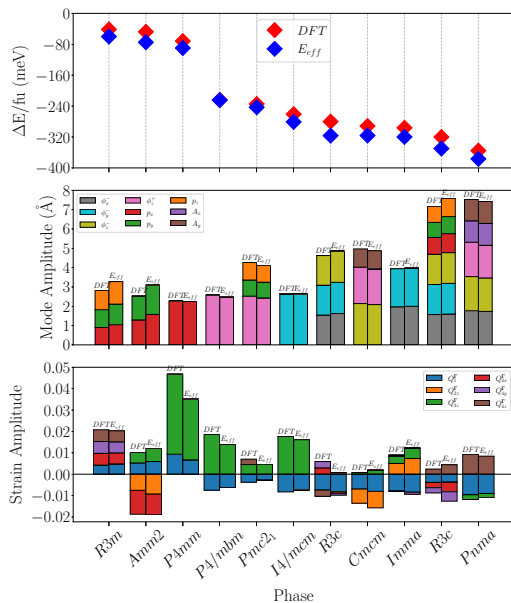
$$r_{xy} = \frac{\sum_i^N (x_i - \bar{x})(y_i - \bar{y})}{\sqrt{\sum_i^N (x_i - \bar{x})^2} \sqrt{(\sum_i^N y_i - \bar{y})^2}}$$

- 1 Model definition
- 2 Training set generation
- 3 Model Generation & Fit
- 4 **Testing/validation**
 - Training set reproduction
 - Relaxations
 - Phonon dispersion curves
- 5 Predictions & analysis tools

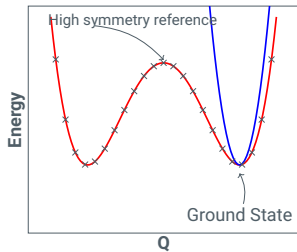
Training set reproduction

Energy difference: DFT vs. Model.

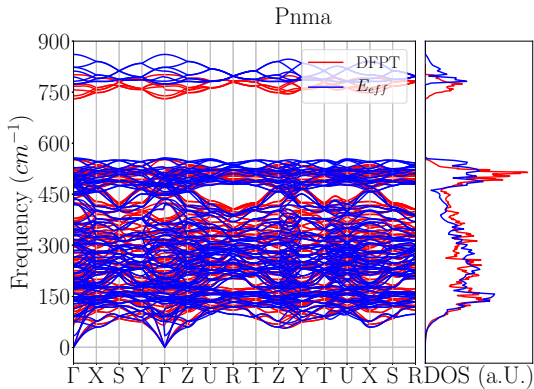
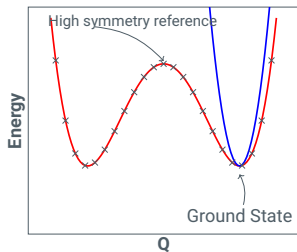




Phonon dispersion curves



Phonon dispersion curves



- 1 **Model definition**

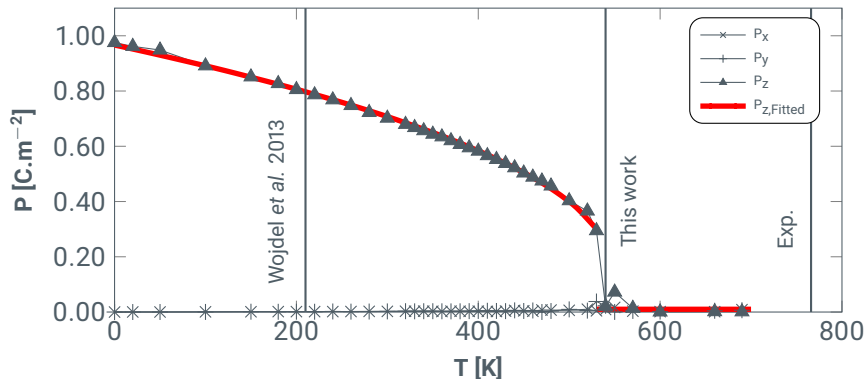
- 2 **Training set generation**

- 3 **Model Generation & Fit**

- 4 **Testing/validation**

- 5 **Predictions & analysis tools**

 - Lead titanate (PbTiO_3)
 - Calcium titanate (CaTiO_3)



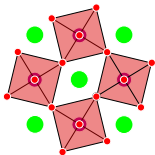
- T_c in better agreement with experiment than previous work
- **First order** phase transition:
 - ▶ Discontinuity at T_c
 - ▶ $P \sim (T_c - T)^{1/4}$

Command in AGATE

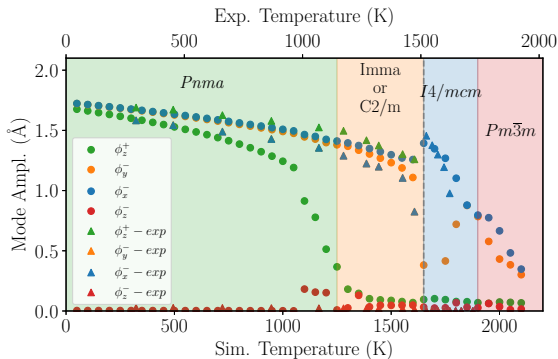
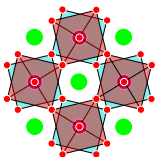
- :average
- :plot xy x=T y="polarization ddb=."

16x16x16 cells, 20480 atoms
Hybrid Monte Carlo Sampling
40000 steps per temperature

In-Phase Rotation ϕ_z^+



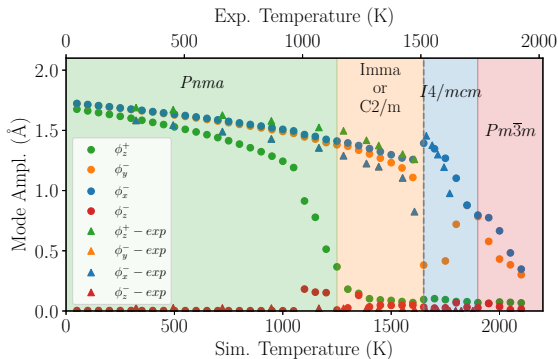
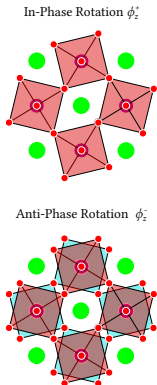
Anti-Phase Rotation ϕ_z^-



Experimental Transitions: $Pnma \rightarrow 1512K \ I4/mcm \rightarrow 1636K \ Pm\bar{3}m$

Yashima, M. & Ali, R., Solid State Ionics, 2009, **180**, 120 - 126

16x16x16 cells, 20480 atoms
Hybrid Monte Carlo Sampling
40000 steps per temperature



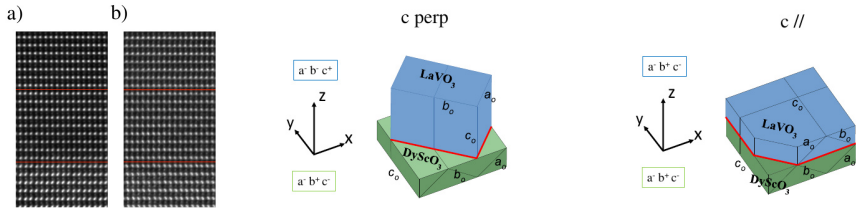
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Yashima, M. & Ali, R., Solid State Ionics, 2009, **180**, 120 - 126

→ But phase transition sequence debated. *Imma* intermediate has been proposed

Carpenter M., American Mineralogist (2007) **92** (2-3): 309-327

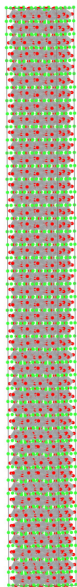
Pnma thin films $\text{LaVO}_3/\text{DyScO}_3$ interface

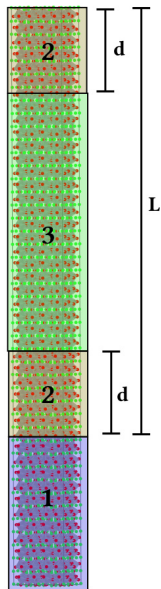


- Thin films (<60 u.c.): only c //.
- Thick films (>60 u.c.): Mostly c perp. but intermediate layer of about 10 u.c. c //.
- Elastically favored c perp.

→ Competition between elastic and interface energy at the origin of intermediate layer formation.

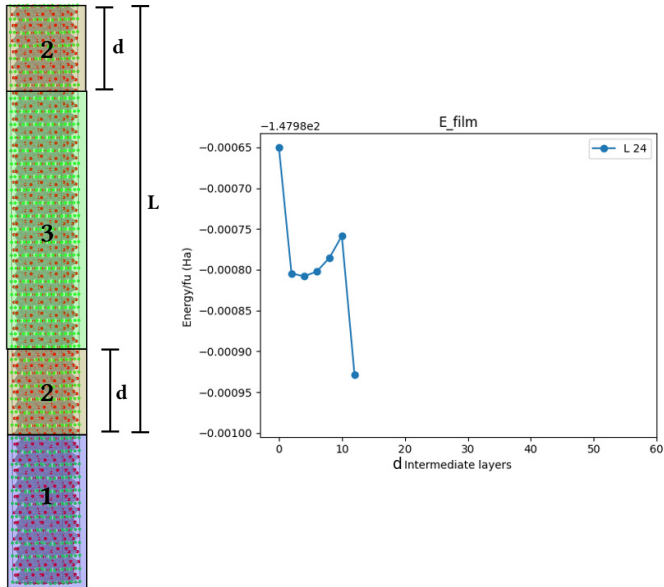
CaTiO₃ Reproduction of LaVO₃/DyScO₃ interface



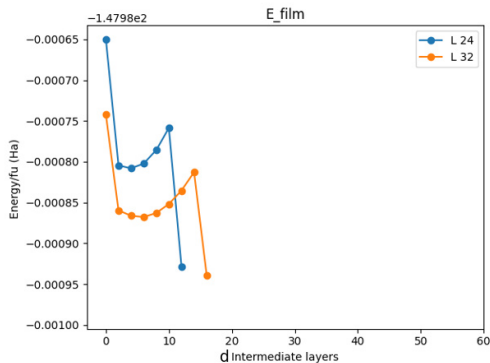
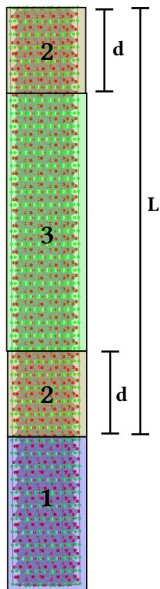


- 1: "substrate" c || with exaggerated distortions
- 2: c || free to relax
- 3: c perp free to relax

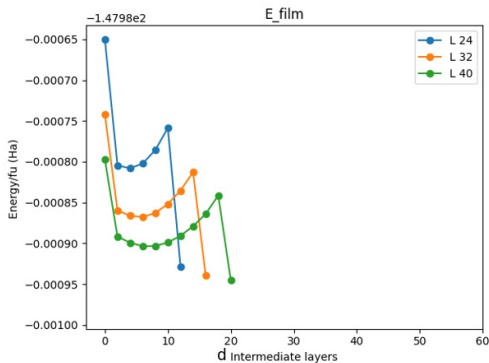
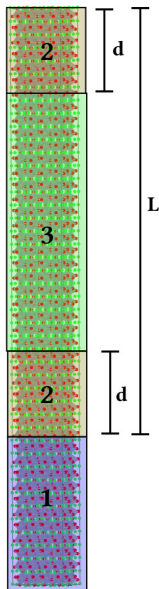
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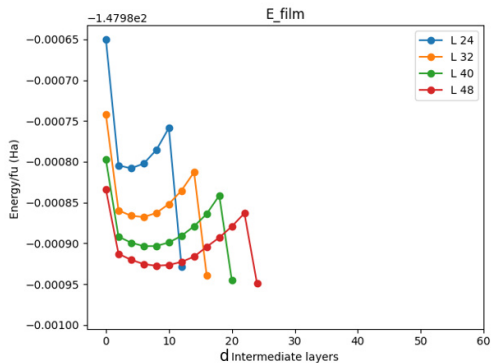
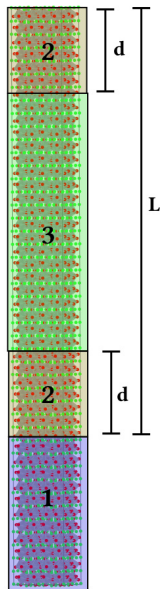
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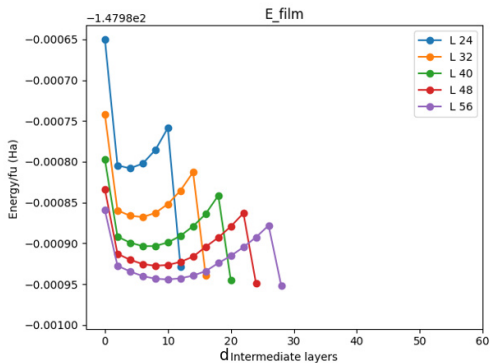
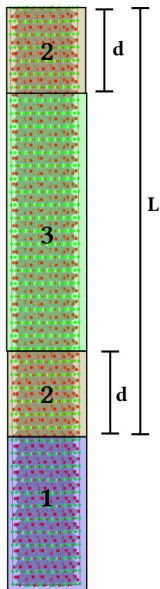
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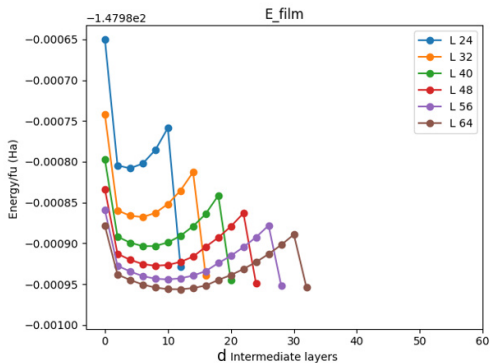
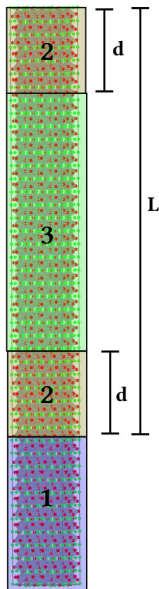
CaTiO₃ Reproduction of LaVO₃/DyScO₃ interface



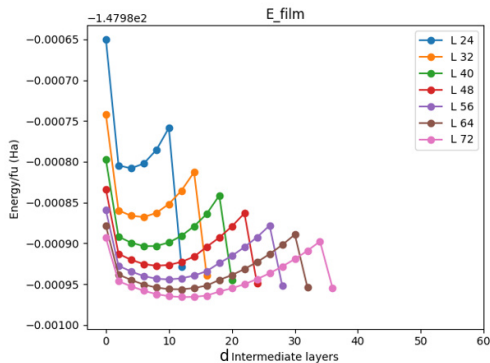
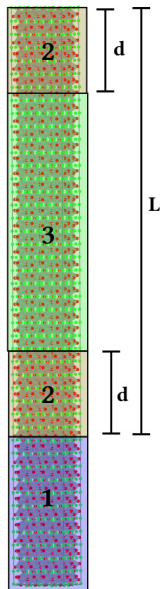
CaTiO₃ Reproduction of LaVO₃/DyScO₃ interface



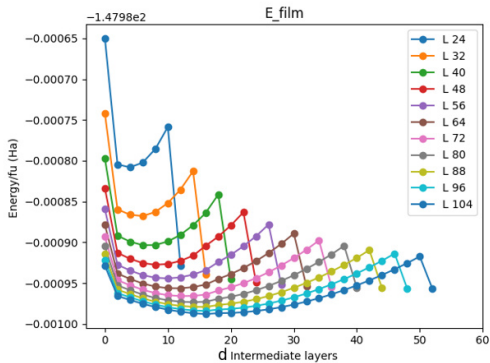
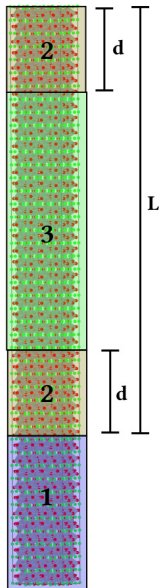
CaTiO₃ Reproduction of LaVO₃/DyScO₃ interface



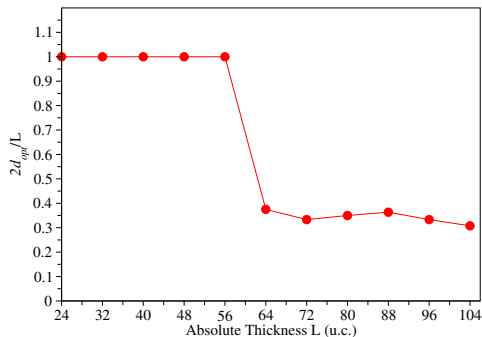
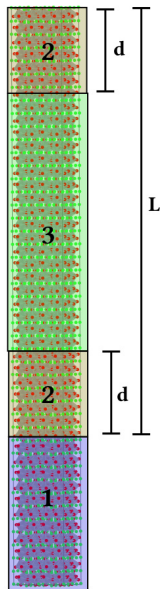
CaTiO₃ Reproduction of LaVO₃/DyScO₃ interface



CaTiO₃ Reproduction of LaVO₃/DyScO₃ interface



CaTiO₃ Reproduction of LaVO₃/DyScO₃ interface



→ CaTiO₃ second-principles model is able to qualitatively reproduce intermediate layer formation at LaVO₃/DyScO₃ interface.

Summary

- Automated procedure for generating fitting polynomial expansions
- New test set generation strategy can help to effectively sample **important** parts of the Born-Oppenheimer PES
- Use of effective potentials for finite temperature and advanced thin film studies.

Outlook

- Implementation of combining different effective potentials in different zones of the simulation box
- New fitting strategies borrowed from machine learning.
- Effective Potentials as background lattice model for electron-lattice, or spin-lattice models